
BIN METHOD FOR THE RATING OF SOLAR COOLING



Matthias Schicktanz

Fraunhofer Institute for Solar Energy
Systems ISE

Task 48 Meeting

Newcastle (Australia), 2013-04-09

www.ise.fraunhofer.de

AGENDA

- Background electrical chillers and motivation
- Results of the project „proposal for a DIN-standard solar cooling“
- Bin-Method procedure for solar cooling

Background

- EU Directive Nr. 206/2012 for compression chillers uses the bin method
 - Definition of a frequency distribution for hours per temperature (reference weather)

j #	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24
T_j °C	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40
h_j h	205	227	225	225	216	215	218	197	178	158	137	109	88	63	39	31	24	17	13	9	4	3	1	0

- Definition of reference cooling load profile

$$P_c(T_j) = \text{part load} = \text{design load} \times \text{part load ratio} = P_{\text{designC}} \times \frac{T_j - 16}{T_{\text{designC}} - 16}$$

- Measurement of the electric chiller performance at 4 bins

Background

■ Result: Energy label

A+++	$\text{SCOP} \geq 5,10$	$\text{SEER} \geq 8,50$
A++	$4,60 \leq \text{SCOP} < 5,10$	$6,10 \leq \text{SEER} < 8,50$
A+	$4,00 \leq \text{SCOP} < 4,60$	$5,60 \leq \text{SEER} < 6,10$
A	$3,40 \leq \text{SCOP} < 4,00$	$5,10 \leq \text{SEER} < 5,60$
B	$3,10 \leq \text{SCOP} < 3,40$	$4,60 \leq \text{SEER} < 5,10$
C	$2,80 \leq \text{SCOP} < 3,10$	$4,10 \leq \text{SEER} < 4,60$
D	$2,50 \leq \text{SCOP} < 2,80$	$3,60 \leq \text{SEER} < 4,10$
E	$2,20 \leq \text{SCOP} < 2,50$	$3,10 \leq \text{SEER} < 3,60$
F	$1,90 \leq \text{SCOP} < 2,20$	$2,60 \leq \text{SEER} < 3,10$
G	$\text{SCOP} < 1,90$	$\text{SEER} < 2,60$

Motivation

Options for solar Cooling:

- create a new solar cooling energy label

Or:

- Stay close to the ecodesign-guideline: „My solar cooling system operates like an A+++ cooling system“
 - stay as close as possible to the EU directive
 - use of the bin Method

Questions:

- Can the reference climate data easily be extended with radiation data?
- How will the calculation method look like?

DIN-Project „Development of a standard for solar cooling“

- Workshop in June 2012 in Frankfurt
- Compilation of the results
- Road map for a Standard for solar cooling

Proposal for a DIN Standard

Solar cooling – vocabulary, safety, measurement procedure, performance evaluation

- Part 1: Vocabulary
- Part 2: General requirements
- Part 3: Safety requirements
- Part 4: Test requirements
- Part 5: Test procedure
- Part 6: Calculation of Seasonal Performance figures

Scope of appliance

- Solar cooling kits (collector, hot water storage, chiller)
- Integrated or separate heat rejection unit
- Open or closed cooling tower
- With or without DHW production
- With or without chilled water storage
- With or without space heating
- Distribution system: chilled water systems, systems for cooling ceilings, systems for fan coils, systems for air ducts
- Solar cooling kits with or without electrical backup
- Solar cooling kits with or without thermal backup

Proposed procedure for the bin-Method

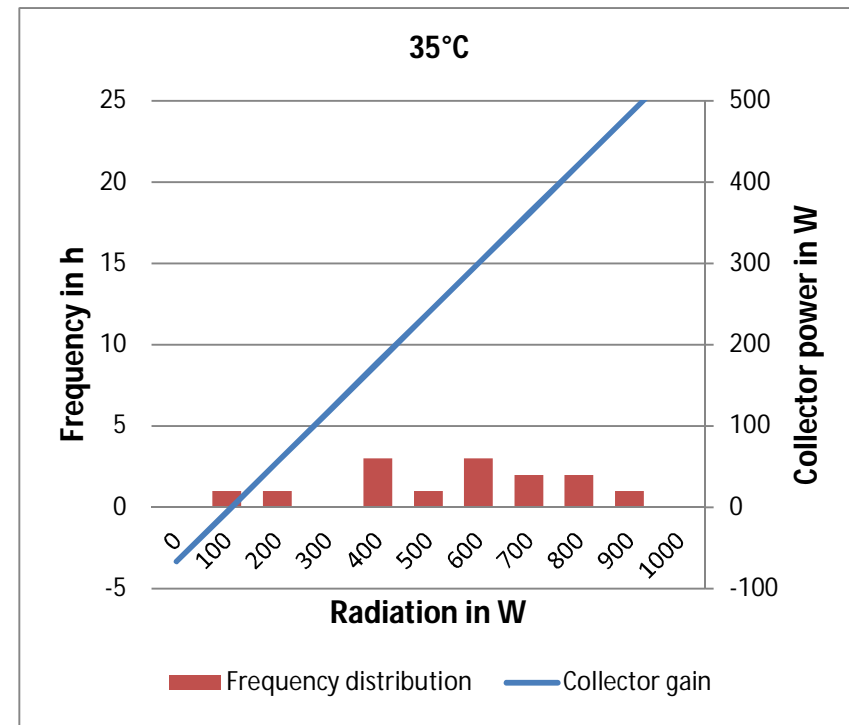
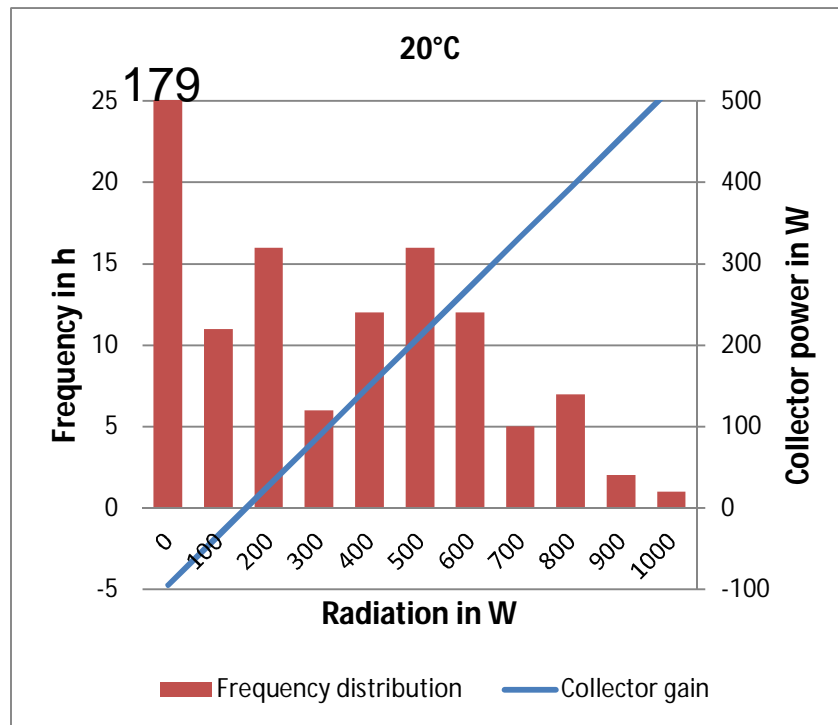
1. Calculate collector gain potential from collector efficiency curve
2. Calculate rejected heat due to filled storage
3. Calculate heat losses from storage UA-value
4. Calculate produced cold from measured EER_{th} and compare to cold demand
→ $SEER_{th}$
→ solar fraction
5. Calculate required electricity from measured EER_{el}
→ $SEER_{el}$

Proposed procedure for the bin-Method

1. Calculate collector gain potential from collector efficiency curve
2. Calculate rejected heat due to filled storage
3. Calculate heat losses from storage UA-value
4. Calculate produced cold from measured EER_{th} and compare to cold demand
→ $SEER_{th}$
→ solar fraction
5. Calculate required electricity from measured EER_{el}
→ $SEER_{el}$

Requirement

- Definition of reference solar radiation and distribution



Calculation of solar gain

- Collector efficiency curve

$$\eta = \eta_0 - \frac{a_1}{G} \times (T_{col} - T) - \frac{a_2}{G} \times (T_{col} - T)^2 = \eta_0 - \frac{P_2(T_{col}, T)}{G}$$

- Collector gain potential

$$P_{col} = \begin{cases} G \times \eta_0 - P_2(T) & G > G_{mini} \\ 0 & \text{else} \end{cases}$$

- Solar gain for temperature T

$$Q_{col,T} = \int_{G_{mini}}^{G_{maxi}} f_T(G) \times P_{col} dG$$

$$Q_{col,T} = \eta_0 \times \int_{G_{mini}}^{G_{maxi}} f_T \times G dG + P_2(T) \times \int_{G_{mini}}^{G_{maxi}} f_T dG$$

Calculation of solar gain 2

■

$$Q_{col,T} = \eta_0 \times \int_{G_{mini}}^{G_{maxi}} f_T \times G \, dG - P_2(T) \times \int_{G_{mini}}^{G_{maxi}} f_T \, dG$$

Collector
Collector

Climate (hours per bin)
Climate (solar radiation per bin)

- Separation of climate key figures and collector parameters possible
- Influence of G_{mini} causes an error in the range of 1%

Bin-Method for solar cooling

- One additional column (solar radiation) is necessary and sufficient to describe the reference climate conditions
- Multiply losses P_2 with hours and η_0 with energy
- Uncertainty is within 1%
- For flat plate and vacuum tube collectors

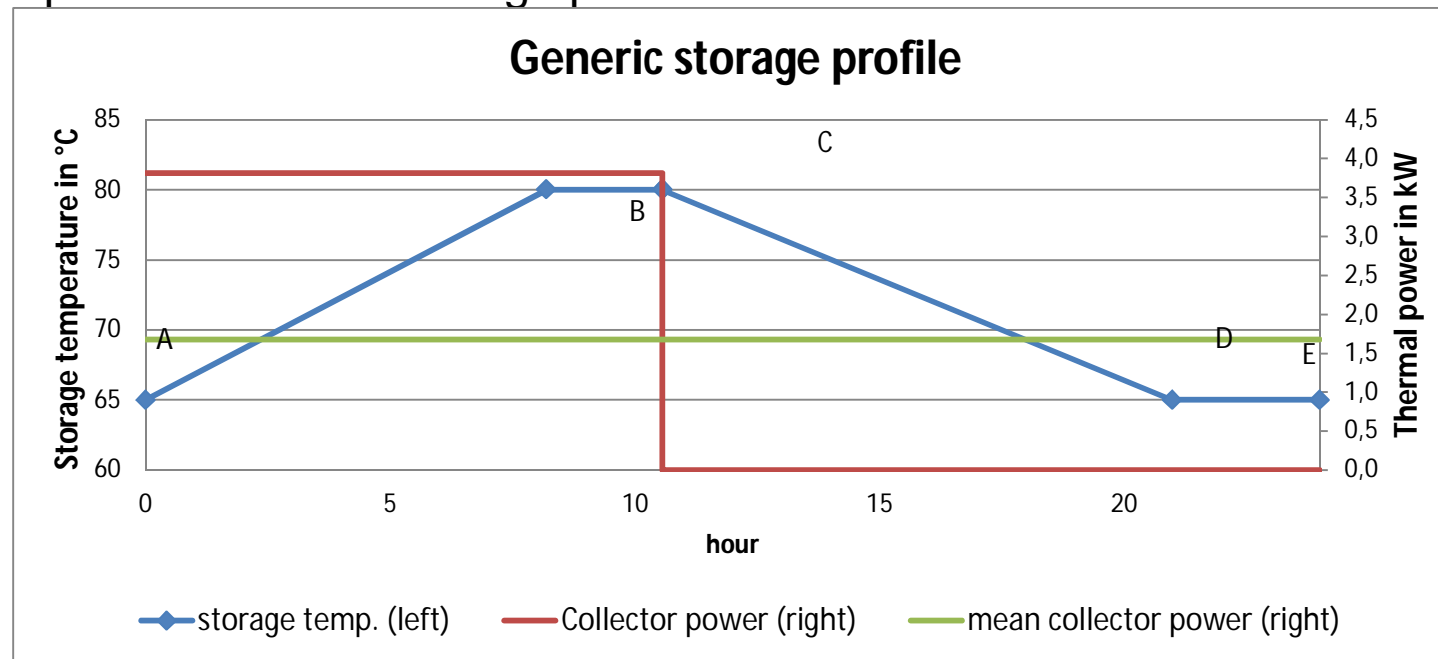
Bin #	Temperature °C	Hours h	Energy kWh
1	16	117	9,5
2	17	170	12,7
3	18	199	17,2
4	19	262	29,4
5	20	267	37,4
6	21	303	51,2
7	22	316	54,7
8	23	354	71,2
9	24	361	84,7
10	25	345	84,4
11	26	321	110,2
12	27	271	97,9
13	28	237	92,8
14	29	169	70,3
15	30	158	75,1
16	31	115	56,4
17	32	85	44,5
18	33	49	26,4
19	34	30	17,0
20	35	14	7,7
21	36	2	1,1
22	37	3	2,0

Proposed procedure for the bin-Method

1. Calculate collector gain potential from collector efficiency curve
2. Calculate rejected heat due to filled storage
3. Calculate heat losses from storage UA-value
4. Calculate produced cold from measured EER_{th} and compare to cold demand
→ $SEER_{th}$
→ solar fraction
5. Calculate required electricity from measured EER_{el}
→ $SEER_{el}$

Correlation of collector and storage

- Option 1: tables from simulation
- Option 2: Generic storage profile



- Output: mean temp. → heat losses full storage → rejected heat

Proposed procedure for the bin-Method

1. Calculate collector gain potential from collector efficiency curve
2. Calculate rejected heat due to filled storage
3. Calculate heat losses from storage UA-value
4. Calculate produced cold from measured EER_{th} and compare to cold demand
→ $SEER_{th}$
→ solar fraction
5. Calculate required electricity from measured EER_{el}
→ $SEER_{el}$

Excel table

Bin	Temperature	hours	radiation (direct)	radiation (diffus)	specific collector gain	collector gain potential	collector efficiency	collector power	collector gain	cold demand	cooling energy	heat demand	COP_Th	COP_el	estimated heat load	storage acceptance	storage efficiency	Heat load	Heat produced	Domestic hot water				Heat for cooling	Cooling power	cooling energy	Used cooling power	used cooling energy	Solar fraction	Solar fraction	electric power	electric energy	uncoverd hours
																				DHW Power	DHW Energy	Solar fraction	solar fraction in hours										
°C	---	W/m ²	W/m ²	kWh/m ²	kW	---	kW	kWh	kW	kWh	kW	JAZ _{Th}	JAZ _{el}	kW	kW	kWh	kWh	kW	kWh	kWh	kWh	kWh	%	h	kW	kWh	h						
1	15	0	0		785,9			2951	1931		0,20	0	0,55	7	1,000	0,000				224,1	26%	1097,8			656	656	26%	1098	142,37				
2	16	0	0	0	0,0	0,0000	0,00	0	0,00	0	0,20	1	0,55	7	1,000	0,000	0,00			0,000	0,000	26%											
3	17	117	46	32	5,4	0,50	-0,1457	0,00	0	0,05	6	0,30	2	0,55	7	1,000	0,000	0,00	0,0	0,000	0,000	0%	0,0	0,000	0,000	0,0	0,00	0,00	0%	0,0	0,000	0,00	117,0
4	18	170	56	36	9,5	0,59	-0,0130	0,00	0	0,11	18	0,40	3	0,55	7	1,000	0,000	0,00	0,0	0,000	0,000	0%	0,0	0,000	0,000	0,0	0,00	0,00	0%	0,0	0,000	0,00	170,0
5	19	199	69	49	13,7	0,75	0,1515	0,09	18	0,16	31	0,49	4	0,55	7	1,000	0,000	0,00	0,0	0,000	0,000	0%	0,0	0,000	0,000	0,0	0,00	0,00	0%	0,0	0,000	0,00	199,0
6	20	262	84	59	22,0	0,92	0,2518	0,18	48	0,21	55	0,59	5	0,55	7,00	1,000	0,000	0,00	0,0	0,000	0,000	0%	0,0	0,000	0,000	0,0	0,00	0,00	0%	0,0	0,000	0,00	262,0
7	21	267	107	64	28,6	1,10	0,3288	0,29	77	0,26	70	0,69	1	0,54	6,8	1,000	0,123	0,04	9,5	0,010	2,798	5%	13,7	0,025	0,014	3,6	0,01	3,61	5%	13,7	0,002	0,53	253,3
8	22	303	112	64	33,9	1,13	0,3459	0,31	95	0,32	96	0,80	2	0,53	6,6	1,000	0,246	0,08	23,3	0,020	5,940	10%	29,1	0,057	0,030	9,2	0,03	9,19	10%	29,1	0,005	1,39	273,9
9	23	316	136	68	43,1	1,31	0,3970	0,42	131	0,37	116	0,91	3	0,52	6,4	1,000	0,369	0,15	48,5	0,034	10,840	17%	53,1	0,119	0,062	19,6	0,06	19,56	17%	53,1	0,010	3,06	262,9
10	24	354	158	82	56,0	1,53	0,4429	0,54	193	0,42	149	1,03	4	0,51	6,2	1,000	0,492	0,27	94,8	0,053	18,792	26%	92,0	0,215	0,109	38,8	0,11	38,75	26%	92,0	0,018	6,25	262,0
11	25	361	161	91	58,0	1,61	0,4585	0,59	213	0,47	171	1,15	5	0,50	6,00	1,000	0,615	0,36	131,0	0,064	23,232	32%	113,8	0,299	0,149	53,9	0,15	53,90	32%	113,8	0,025	8,98	247,2
12	26	347	228	117	79,0	2,21	0,5196	0,92	318	0,53	183	1,30	1	0,48	5,6	0,981	0,654	0,59	204,3	0,092	32,075	45%	157,1	0,496	0,238	82,7	0,24	82,69	45%	157,1	0,043	14,77	189,9
13	27	321	231	132	74,1	2,32	0,5308	0,99	317	0,58	186	1,46	2	0,46	5,2	0,962	0,693	0,66	211,2	0,092	29,477	45%	144,4	0,566	0,260	83,6	0,26	83,59	45%	144,4	0,050	16,07	176,6
14	28	271	250	146	67,7	2,53	0,5453	1,10	299	0,63	171	1,64	3	0,44	4,8	0,943	0,732	0,76	206,5	0,095	25,711	46%	125,9	0,667	0,293	79,5	0,29	79,54	46%	125,9	0,061	16,57	145,1
15	29	237	280	141	66,4	2,70	0,5560	1,20	284	0,68	162	1,83	4	0,42	4,4	0,924	0,771	0,85	202,4	0,095	22,539	47%	110,4	0,759	0,319	75,5	0,32	75,53	47%	110,4	0,072	17,17	126,6
16	30	169	317	158	53,6	3,04	0,5716	1,39	235	0,74	125	2,05	5	0,40	4,00	0,904	0,810	1,02	172,2	0,102	17,179	50%	84,1	0,917	0,367	62,0	0,37	62,00	50%	84,1	0,092	15,50	84,9
17	31	158	346	150	54,6	3,17	0,5782	1,47	232	0,79	125	2,40	1	0,36	3,8	0,898	0,815	1,07	169,8	0,092	14,460	45%	70,8	0,983	0,354	55,9	0,35	55,92	45%	70,8	0,093	14,71	87,2
18	32	115	385	148	44,2	3,41	0,5870	1,60	184	0,84	97	2,84	2	0,32	3,6	0,892	0,821	1,17	135,0	0,084	9,717	41%	47,6	1,089	0,348	40,1	0,35	40,08	41%	47,6	0,097	11,13	67,4
19	33	86	401	142	34,5	3,48	0,5908	1,64	141	0,89	77	3,40	3	0,28	3,4	0,886	0,826	1,20	103,6	0,072	6,219	35%	30,5	1,132	0,317	27,3	0,32	27,25	35%	30,5	0,093	8,02	55,5
20	34	49	436	140	21,3	3,68	0,5973	1,76	86	0,95	46	4,15	4	0,24	3,2	0,880	0,832	1,29	63,1	0,063	3,104	31%	15,2	1,225	0,294	14,4	0,29	14,40	31%	15,2	0,092	4,50	33,8
21	35	30	417	134	12,5	3,52	0,5962	1,68	50	1,00	30	5,20	5	0,20	3,00	0,874	0,837	1,23	36,9	0,048	1,447	24%	7,1	1,181	0,236	7,1	0,24	7,09	24%	7,1	0,079	2,36	22,9
22	36	14	479	94	6,7	3,66	0,6011	1,76	25	1,05	15	6,78	1	0,16	2,4	0,874	0,837	1,29	18,0	0,039	0,543	19%	2,7	1,250	0,200	2,8	0,20	2,80	19%	2,7	0,083	1,17	11,3
23	37	2	547	97	1,1	4,12	0,6106	2,01	4	1,11	2	9,41	2	0,12	1,8	0,874	0,837	1,47	2,9	0,032	0,064	16%	0,3	1,441	0,173	0,3	0,17	0,35	16%	0,3	0,096	0,19	1,7
24	38	0	0	0	0,0	0,0000	0,00	0	0	1,16	0	14,68	3	0,08	1,2	0,874	0,837	0,00	0,0	0,000	0,000	0%	0,0	0,000	0,000	0,0	0,00	0,00	0%	0,0	0,000	0,00	0,0
25	39	0	0	0	0,0	0,0000	0,00	0	1,21	0	30,47	4	0,04	0,6	0,874	0,837	0,00	0,0	0,000	0,000	0%	0,0	0,000	0,000	0,0	0,00	0,00	0%	0,0	0,000	0,00	0,0	
26	40	0	0	0	0,0	0,0000	0,00	0	1,26	0	#DIV/0!	5	0,00	0,00	0,874	0,837	0,00	0,0	0,000	0,000	0%	0,0	0,000	0,000	0,0	0,00	0,00	0%	0,0	0,000	0,00	0,0	

■ Output: El. SCOP, Th. SCOP, solar fraction

Strength and weakness

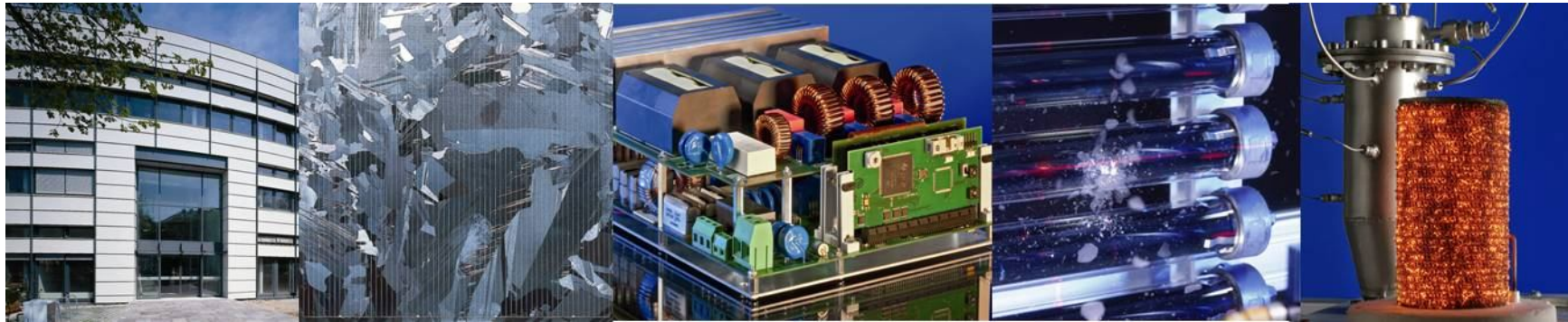
■ Strength:

- Simple method
- No simulation-license required
- Transparent to the user
- Very close to the compression chiller marked
- Required parameters have a physical meaning
- Only TDC-performance measurement at 4 points required (no system measurement required)

■ Weakness:

- Control issues not regarded (also true for CTSS)
- On/off behaviour not yet regarded
- Collector/storage behaviours must be analyzed
- Additional radiation table for concentrating systems required

Thank you for your attention!



Fraunhofer Institute for Solar Energy Systems ISE

Matthias Schick Tanz

www.ise.fraunhofer.de

Matthias.schick Tanz@ise.fraunhofer.de

Elements of a standard for solar cooling

